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ABSTRACT

This report covers the period of the contract extension, from 1 September 1979 to 31 August 1980. Tasks established and carried out during this period were: the development of a general ray trace evaluation program, called ICARUS; the study of novel Fresnel concepts; and the review of a report draft on novel Fresnel concepts. ICARUS is documented herein; reports on the novel Fresnel concepts have been submitted earlier.

NEW TECHNOLOGY

Fresnel Computation Program

A general ray trace evaluation program, designated ICARUS, has been developed, with the goal of widening the generality over that in commercially available optical evaluation programs. The main thrust of the effort has been to expand the number of geometrical shapes, tilts, and decenters that could be explored, to include conic, aspheric, and toric surfaces. To keep the program task within time and budget, the effect of facet errors was not to be included. This task has been performed principally by Steve Eckhardt, graduate student, under the supervision of A. B. Meinel. Documentation is appended to this report (Appendix A).

A review of the program led to the decision by us and by JPL's program management to terminate this task before completion; however, we were able to bring it to a usable state; examples of Fresnels that can be ray traced are shown in Appendix B. One reason for withdrawing

from the hope of a fully general program was the conclusion that a specific program could be written for any novel Fresnel surface that could not be handled by an existing program.

It is important to know what has not been included in the program to date. Not included are the following capabilities: (1) finite groove size, (2) diffraction, (3) local groove effects (facet tilt error), (4) substrate effects (lens surface errors), and (5) general aspheric substrate shapes. The facet tilt error and surface errors are relatively easy to handle for reflective Fresnels in that whatever the angular distribution of assumed errors is, the effect at the focus is twice the angular distribution, subject to the geometrical cosine effect of oblique incidence on the focal plane. The effect is considerably more complicated for refractive Fresnels. We will examine the analytical expressions in future work if JPL requests it.

Questions of adding facet error statistics have yet to be incorporated. The analytical approaches to this are currently being evaluated and could appear as an addendum at the appropriate time.

Fresnel Optic Study

The rest of the current funding was expended in addressing novel Fresnel concepts, on which reports have been submitted, and in reviewing a report draft on this topic prepared by JPL. Several of the novel concepts appear to be patentable, and a report was written on this question, but no reply was received concerning JPL's desire to proceed with this question. In the absence of a reply we will, at an appropriate time, prepare a paper for journal publication on these novel concepts.

APPENDIX A

PROGRAM DOCUMENTATION

PROGRAM IDENTIFICATION

Program Title: Optical Sciences Center Fresnel Evaluation Program

Program Code Name: ICARUS

Writer: Steve Eckhardt
Optical Sciences Center
University of Arizona
Tucson, Arizona 85721

Date of Completion: May 1980

Source Language: Fortran (Data General FORTRAN 5)

Availability: Program listing as computer printout (attached)

Abstract: ICARUS is a ray trace program of greater generality than commercially available programs.

PROGRAM DESCRIPTION

Method of Solution: Paraxial rays are traced by normal methods. Real rays are traced in accordance with the conic ray trace equations given in Table 1. Fresnels are treated by assuming that the point of intersection of the ray with the surface is in the tangent plane of the lens and that the angle of the normal to the ray is the same as if the Fresnel were an ordinary conic.

Program Capabilities: Paraxial and real ray tracing, as well as radiant energy distribution computation, for conic, fresnel, toric, curved fresnel, toric fresnel, and curved toric fresnel surfaces. Not included are finite groove size, diffraction, local groove effects (facet tilt error), substrate effects (lens surface errors), and general aspheric substrate shapes.

Data Inputs:	Data are entered interactively at the terminal, in response to questions posed by the program. Tables 3 and 4 provide guides to input options and format.
Program Options:	See Table 3
Printed Output:	N/A
Other Outputs:	A file is created for each new lens. These can only be deleted outside of the program.
Flow Chart:	Figure 1 is a general system flow chart.
Sample Run:	Table 3 is an annotated "walk-through" of the program.

SYSTEM DOCUMENTATION

Computer Equipment:	Data General Eclipse
Peripheral Equipment:	N/A
Source Program:	Table 5 is a complete source code listing for ICARUS and its subroutines.
Variables and Subroutines:	See the source code listing for variables. Table 2 is a list of subroutines, with descriptions of their functions.
Data Structures:	N/A
Storage Requirements:	Minimal
Maintenance and Updates:	None

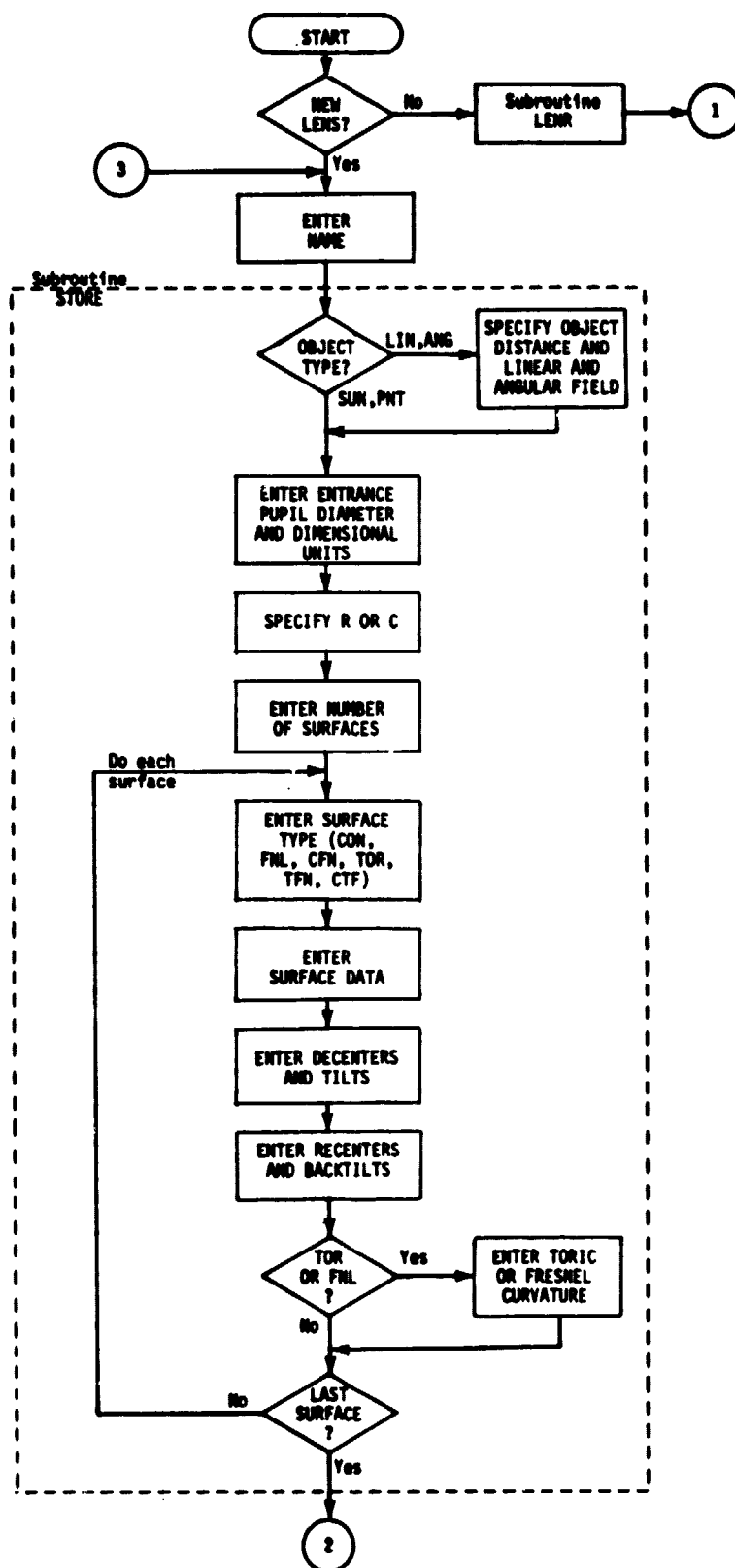


Fig. 1. ICARUS System Flow Chart

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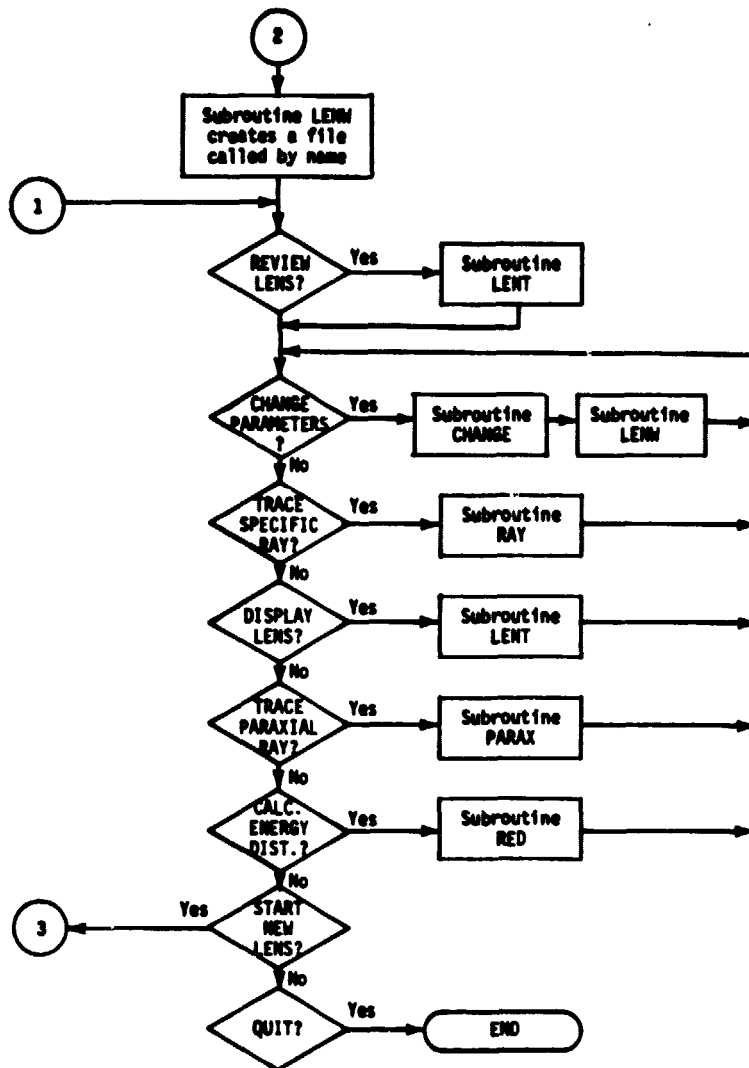


Fig. 1. ICARUS System Flow Chart (Continued).

Table 1. Ray Trace Equations for Conics.

Opening:

$$\begin{aligned} A &= [t^2 + (h_y - y_t)^2 + (h_x - x_t)^2]^{1/2} \\ L &= \frac{h_x - x_t}{A} \\ M &= \frac{h_y - y_t}{A} \\ N &= t/A \end{aligned}$$

Transfer to Surface:

$$\begin{aligned} B &= c(x_t^2 + y_t^2) \\ C &= N - c(Lx_t + My_t) \\ D &= [C^2 - cB(1 + kN^2)]^{1/2} \quad \underline{D^2 < 0: \text{ ray missed surface}} \\ A &= B/(C + D) \\ x_s &= x_t + AL \\ y_s &= y_t + AM \\ z_s &= AN \end{aligned}$$

Refraction:

$$\begin{aligned} E &= [1 - 2ckz_s]^{-1/2} \\ \cos I &= DE \\ \mu &= n/n' \\ \delta &= (1 - \mu^2 + \mu^2 \cos^2 I)^{1/2} - \mu \cos I \\ &\quad \underline{1 - \mu^2 + \mu^2 \cos^2 I < 0:} \\ &\quad \underline{\text{total internal reflection}} \end{aligned}$$

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Table 1. Ray Trace Equations for Conics (Continued).

$$\begin{aligned}\alpha &= -cE x_s \\ \beta &= -cE y_s \\ \gamma &= [1 - C(k+1)z_s]E \\ L' &= \mu L + \delta\alpha \\ M' &= \mu M + \delta\beta \\ N' &= \mu N + \delta\gamma\end{aligned}$$

Transfer to Tangent Plane:

$$\begin{aligned}x_t &= x_s + L(t - z_s)/N \\ y_t &= y_s + M(t - z_s)/N \\ A &= [(t - z_s)^2 + (y_t - y_s)^2 + (x_t - x_s)^2]^{1/2}\end{aligned}$$

Variable Definitions:

$$\begin{aligned}x_t &= \text{ray height in } x \text{ on tangent plane} \\ y_t &= \text{ray height in } y \text{ on tangent plane} \\ x_s &= \text{ray height in } x \text{ on surface plane} \\ y_s &= \text{ray height in } y \text{ on surface plane} \\ t &= \text{distance from object to first lens surface, or distance} \\ &\quad \text{between surfaces} \\ h_x &= \text{object height in } x \\ h_y &= \text{object height in } y \\ L, M, N &= x, y, z \text{ direction cosines for the ray before refraction} \\ L', M', N' &= x, y, z \text{ direction cosines for the ray after refraction} \\ \alpha, \beta, \gamma &= \text{direction cosines of the normal to the surface in } x, y, \\ &\quad \text{and } z, \text{ respectively} \\ A &= \text{geometrical path length between a surface and the following} \\ &\quad \text{tangent plane; also vice versa, the refractive index times} \\ &\quad \text{the optical path length} \\ I &= \text{the angle of incidence on the surface} \\ n, n' &= \text{the refractive indices of the materials before and after} \\ &\quad \text{the surface} \\ B, C, D, E, \delta &= \text{dummy variables}\end{aligned}$$

Table 2. List of Subroutines.

Name	Called by	Description
CHANGE	Main program	Interacts with user to make individual changes in the lens without requiring re-typing of entire lens; inputs are as in subroutine STORE
LENR (lens read)	Main program, PARAX	Reads a currently existing lens file into the active area
LENT (lens type)	Main program	Displays the current lens on the terminal in tabular form
LENW (lens write)	CHANGE, STORE	Creates a file called by any name the user specifies, and writes the lens to it. Should the need arise, this file may be accessed for modification without use of the program
PARAX	Main program	Does a paraxial ray trace that enables the user to locate the Gaussian image plane, and in general to do a rough lens design
RAY	Main program, RED	Traces a specified ray through the lens (see TORT and SYMM)
RED	Main program	Calculates the radial energy distribution in the image plane
SORT	RED	Orders the rays by increasing radial distance from the paraxial image point
STORE	Main program	Interactively accepts data input
SYMM	RAY	Does refraction calculations for symmetrical surfaces
TORT	RAY	Does refraction calculations for toric surfaces
<u>Subroutines Programmed into the Data General Eclipse</u>		
CLOSE	LENR, LENW	Subroutine for closing a file
FOPEN	LENR, LENW	Subroutine for opening a file

Table 3. Walk-Through of ICARUS Program.

To log onto the system:

USER NAME:

SUN [sample user inputs are indicated in this special type face]

PASSWORD:

STEVE [this can be changed]

After much printing, user may execute the program by typing:

MXEQ ICARUS 15 [this is system dependent]

IS THIS A NEW LENS? [Y or N]

Y

WHAT IS ITS NAME? [up to 7 alphanumeric characters]

LENS10 [for example]

If this were not a new lens, the identifier statement would cause subroutine LENR (lens read) to be called; this routine reads in stored lens data from memory.

The following comes from subroutine STORE:

ENTER OBJECT TYPE [the choices are: SUN (specifies sun as the object), PNT (point source), LIN (specifies an object defined in terms of its linear dimensions, ANG (specifies an object defined in terms of angular subtense); entering LIN or ANG triggers the following interactions]

```
-----
|  LIN
|  OBJECT DISTANCE IS:
|    100 [or whatever]
|  LINEAR FIELD(S) =
|    10 5 [height in y and x directions, respectively]
|  -----
```

```
-----
|  ANG
|  OBJECT DISTANCE IS:
|    1000 [or whatever]
|  ANGULAR FIELD(S) =
|    5 0 [subtense in y and x directions, respectively; angles are
|        in degrees]
|  -----
```

SUN

ENTER ENTRANCE PUPIL DIAMETER [currently only circular optics can be handled; the entrance pupil diameter for most solar collectors will be the collector diameter]

10

ENTER DIMENSIONS [MM or IN or M or CM or FT, etc.; this could be changed to ENTER UNITS. Currently, this is of no use except perhaps to help the designer remember; in the future, program additions could make use of this feature to scale output]

DO YOU WISH TO SPECIFY RADII (R) OR CURVATURES (C)? [R or C: since the program works in curvatures, if R is entered, all curve inputs will be divided into 1 to obtain curvatures; this pertains to surface data, toric curvatures, and Fresnel curvature]

HOW MANY LENS SURFACES ARE THERE? [generally, the answer will be 1, but the program can handle several; this number does not include object or image surfaces; the image is assumed to be plane and normal to the optical axis]

2

ENTER SURFACE TYPE [options are as follows]

CON: a conic section (ellipse, sphere, parabola, hyperbola)

FNL: a normal Fresnel lens; aspheres are permitted

CFN: curved Fresnel, a Fresnel lens that does not lie on a plane; only spherical base curves are permitted

TOR: a toroid, a lens with different curvatures in the x and y directions

TFN: toric Fresnel, a Fresnel with differing x and y curvatures

CTF: curved toric Fresnel, a toric Fresnel that does not lie on a plane; only spherical base curves are permitted

CON

ENTER SURFACE DATA [respectively R, CC, TH, N_1 , N_2 , and N_3 , defined as follows; as in input elsewhere, numbers are separated by a space]

R: radius of curvature or curvature of surface

CC: conic constant: $CC = 0 \rightarrow$ sphere, $CC = -1 \rightarrow$ paraboloid, $CC > 0 \rightarrow$ oblate spheroid, $CC < -1 \rightarrow$ hyperboloid, $0 > CC > -1 \rightarrow$ ellipsoid

TH distance to vertex of next surface

N_1, N_2, N_3 indices of refraction of three wavelengths

200 -2 10 1.523 1.516 1.527

ENTER DECENTERS AND TILTS [respectively XDEC, YDEC (x- and y-decenters in common units), α , β , γ (tilts in degrees); these are currently not operational, but soon to follow are program additions that will incorporate them; since they are currently disregarded by the program, 0 is a good entry]

0 5 0 0 0

1st surface

ENTER RECENTERS AND BACKTILTS [respectively REC_1 , REC_2 , α' , β' , γ' ;
again, these are not currently operational]

□ □ □ □ □

ENTER SURFACE TYPE

CTF

ENTER SURFACE DATA

□ □ 100 1 1

[first two entries negated by choice of surface type; if a nontoric
is requested in preceding line, then the R appears as the first
entry here]

ENTER DECENTERS AND TILTS

□ □ □ □ □

ENTER RECENTERS AND BACKTILTS [same sign as original decenter or tilt
cancels the former]

□ 5 □ □ □

ENTER TORIC CURVATURES [CVX, CVY (x curve and y curve); this question
appears only if a toroid has been specified]

100 210 [curvatures (C) or radii (R), as previously specified]

ENTER CURVATURE OF FRESNEL [base curve; appears if Fresnel is specified]

-150 [curvature (C) or radius (R), as previously specified]

*Subroutine LENW (lens write) is now called; it creates a file called by
the name the user specifies, and writes the lens to it. Should the need
arise, this file may be accessed for modification without using the program.*

Return to main program:

WOULD YOU LIKE TO REVIEW YOUR LENS? [Y or N; Y (yes) triggers subrou-
tine LENT, which displays the tabulated data on the lens; this step
is used to see whether any errors have occurred or whether the de-
signer wants to change anything]

Y

*Subroutine LENT (lens type): displays the current lens on the termi-
nal in tabular form.*

WOULD YOU LIKE TO MAKE ANY CHANGES? [Y or N; Y triggers subroutine
CHANGE, which will then ask for the changes you'd like to make]

Y

*Subroutine CHANGE: interacts with the user to make individual changes
in the lens without having to retype the entire lens; all user inputs
are as in subroutine STORE.*

WHAT WOULD YOU LIKE TO DO NOW? [options are RAY, LENT, CHANGE, PARAX, RED, NEW, QUIT; handled by subroutines described below]

RAY

Subroutine RAY: traces a specified ray through the lens. RAY in turn uses two subroutines, TORT and SYMM, to do the refraction calculations for toric surfaces and axially symmetrical surfaces, respectively. Interaction is as follows:

WHICH COLOR IS THE RAY, 1, 2, or 3? [1, 2, or 3: refers to N_1 , N_2 , and N_3]

ENTER FRACTIONAL OBJECT HEIGHTS [FOBY, FOBX: the normalized (full field = 1) height on the object from which the ray is to start; excluded if the object is SUN]

ENTER FRACTIONAL PUPIL COORDINATES [RHOY, RHOX, the normalized (half of the entrance pupil diameter = 1) ray height on the entrance pupil; can be any coordinates, not the 0.7, 1.0 rays, which are built in when RED is required. The output is as follows:

RAY COORDINATES AT IMAGE PLANE: X = , Y = , R =

$$R = (X^2 + Y^2)^{1/2}$$

LENT

Subroutine LENT (lens type): displays the current lens on the terminal in tabular form.

CHANGE

Subroutine CHANGE: interacts with the user to make individual changes in the lens without having to retype the entire lens; described above.

PARAX

Subroutine PARAX: does a paraxial ray trace that enables the user to locate the Gaussian image plane, and in general to do a rough lens design. One question is asked:

IS THIS IN COLOR 1, 2, or 3? [1, 2, or 3: determines whether N_1 , N_2 , or N_3 is used for each surface in the trace. Output is in the following form:

SURF	AXIAL Y	CHIEF Y	AXIAL U	CHIEF U
0	*****	.	.	.
1
.
.
.

where SURF is the surface number (0 = object; the last surface is the image surface), AXIAL Y represents the height of the ray that passes through the center of the object and the edge of the entrance pupil, CHIEF Y is the height of the ray that passes through the edge of the object and the center of the entrance pupil, AXIAL U is the angle the axial ray makes with the optical axis prior to refraction at specified surface, and CHIEF U is the angle of the chief ray; angles are measured counterclockwise from the axis]

RED

Subroutine RED: calculates the radial energy distribution in the image plane. The object is always assumed to be the sun. Interaction is as follows:

HOW MANY COLORS WOULD YOU LIKE? [1, 2, or 3: If 1 is specified, index N_1 is used and 96 rays are traced through the system. If 2 is specified, 96 additional rays are traced using N_2 at each surface. If 3 is specified, 96 rays are traced using N_3 in addition to those with N_1 and N_2 . To do this, subroutine RAY is used. The radial coordinate in the image plane is then stored, and subroutine SORT is called. This subroutine arranges the points in order of increasing radius, and puts them into 10 bins. Each bin is now assumed to contain 10% of the energy entering the system.]

Output is as follows, where r_n = the radius containing successive percentages of ray intercepts:

PERCENT ENERGY	RADIUS
10	r_1
20	r_2
30	r_3
⋮	⋮
100	r_{10}

NEW [start on a new lens (or a different old one)]

QUIT [terminates the program; to restart it, type MXEQ ICARUS 15 (as before)]

WHAT NEXT? [options are any of the above]

QUIT

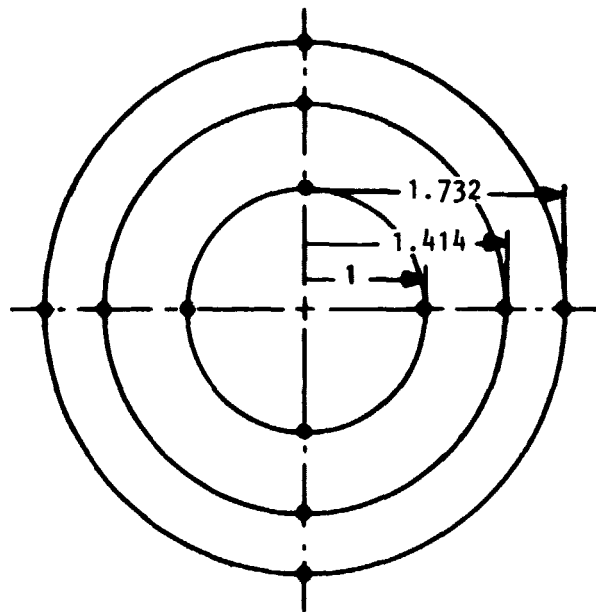
To log off Eclipse:

BYE

Table 4. User's Notes on Program ICARUS.

1. The program takes 12 points to describe the sun, eight points on the lens in up to three wavelengths specified by three indices of refraction. This set then specifies 288 rays. If more points on the lens are desired, it will require recompiling the program and will involve considerably more computation time (unless a single wavelength is desired, thus permitting 24 points on the lens).

The pattern of points on the sun is as shown below. They are distributed in rings of equal area, each ring being weighted for a cosine solar limb-darkening effect. In reality, the power associated with limb darkening should be less than unity for closer approximations to the true sun, but for simplicity we have assumed a $\cos 1.0x$ relationship.



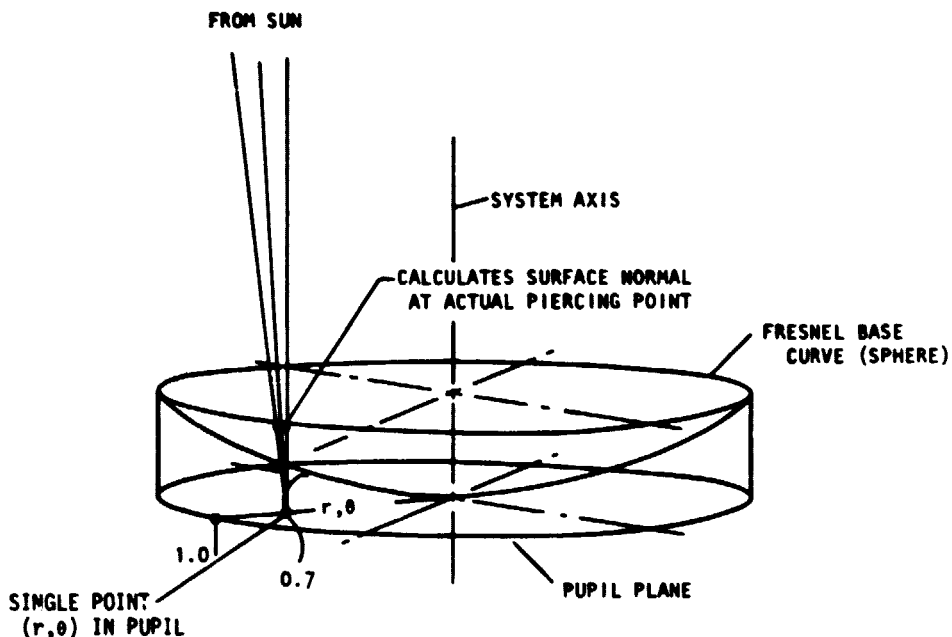
Pattern of points on the sun distributed
in weighted equal-area rings.

2. The choice of surface type encompasses plane and plane tilted (as in the faceted Fresnel panel concept).

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Note that the Fresnel surface has no finite grooves in this analytical program. The proper tilt of the Fresnel element at the point where the entering solar rays reach the lens surface is automatically calculated as discussed below.

The entrance pupil is in a plane normal to the vertex of the Fresnel base curve, as shown below. The present program takes eight rays: two radii ($r = 0.7$ and 1.0 the lens diameter at $\theta =$ each of $0, 90, 180,$ and 270 degrees. No central ray is traced.



Definition of the pupil plane and Fresnel
base (substrate) curve.

The rays from the finite sun are directed to a single point (r, θ) . When the rays are transferred to the specified Fresnel base curve, the r, θ values will be slightly different because the rays from the disc of the sun are tilted with regard to the normal at the pupil surface. The same effect arises from either a tracking error or a deliberate tilt.

The program calculates the normal at its intersection point of the Fresnel surface. The equivalent curvature of the Fresnel optical

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surface is calculated, as illustrated below. The equivalent Fresnel element surfaces are always considered as curved elements, curved to yield a point focus at the specified TH value given for the final optical surface (if more than one is involved).

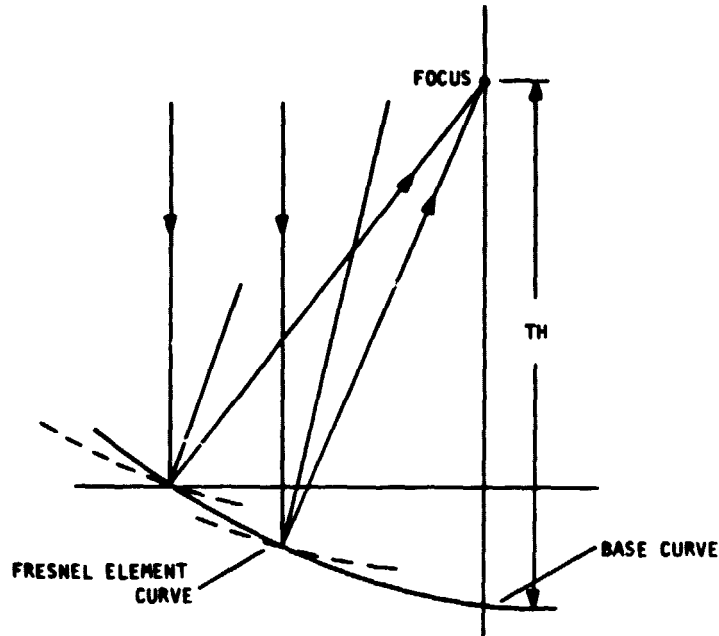


Illustration of the difference between the base (substrate) curvature and the equivalent element curvature.

The "proper tilt" of the Fresnel element has a subtle definition, as illustrated in the next figure. The equivalent Fresnel curvature has a constant value of RD (or CV) and CC, but is shifted by an amount Δ so that the slope at r brings the reflected ray at r to the focus. In other words, the program shifts the conic.

The radius and curvature are defined by the focal length F or the power P , by

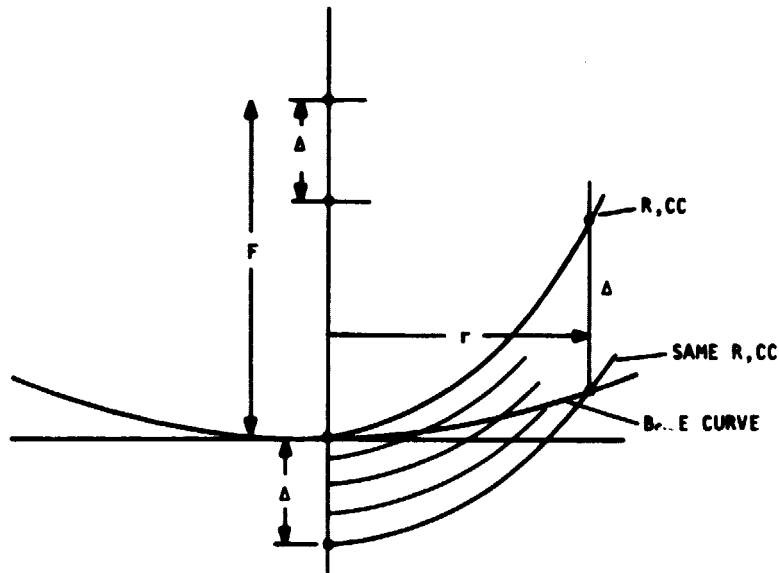
$$CV = P/2$$

$$P = 1/F$$

RD equals $2F$ for a reflector, or

$$\left. \begin{aligned} 1/F &= (n' - n) (1/r_1 - 1/r_2) \\ P &= (n' - n) (CV_1 - CV_2) \end{aligned} \right\} \text{ for a lens.}$$

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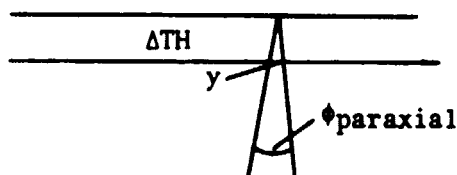
Geometry illustrating the shift in the effective conic surface defining facet angles.

There is a strategy for finding the best value of CC for the equivalent facets, depending on the base surface used. For example, the best value of CC for a plane reflective Fresnel mirror is a hyperboloid, $CC = -3.0$. The strategy is to try a CC and examine the ray distribution in the focal surface, then change CC to find the best distribution.

The curvature is the inverse of the radius of curvature. The conic constant is:

hyperboloid	$CC < -1$
paraboloid	$CC = -1$
ellipse	$-1 \leq CC \leq 0$
sphere	$CC = 0$

3. To find a better value of TH for the focus, take the output value of the y intercept with the TH plane and paraxial angle ϕ , and calculate. Calculate an unproved TH using a pocket calculator.



$$\Delta TH = y\phi$$

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Table 5. Source Code Listing of Program ICARUS.

```

PARAMETER NRAY=96,IP=11,OF=18,NP=2
COMMON/NAME/ANAME,IREC,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,THS
COMMON/SD/SUR(18),CV(18),CC(18),TH(18),N(11,3)
COMMON/TD/DEC(18,2),TILT(18,3),RDEC(18,2),RTILT(18,3),CVY(18),CVX(18)
COMMON/TD/CVF(18)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(18)
COMMON/RAYS/R(NRAY,3)
REAL N,LNX,LNY
LOGICAL LG
18  TYPE"IS THIS A NEW LENS?"
    READ(IP,988) IAGE
    TYPE"WHAT IS ITS NAME?"
    READ(IP,985) ANAME
    IF(IAGE.EQ."Y") CALL STORE
    IF(IAGE.EQ."N") CALL LENR
    TYPE"WOULD YOU LIKE TO REVIEW YOUR LENS?"
    READ(IP,988) LR
    IF(LR.EQ."Y") CALL LENT
    TYPE"WOULD YOU LIKE TO MAKE ANY CHANGES?"
    READ(IP,988) ICQ
    IF(ICQ.EQ."Y") CALL CHANGE
    TYPE"WHAT WOULD YOU LIKE TO DO NOW?"
    READ(IP,985) WORK
28  IF(WORK.EQ."RAY") GOTO 188
    IF(WORK.EQ."LENT") GOTO 118
    IF(WORK.EQ."PARAX") GOTO 128
    IF(WORK.EQ."RED") GOTO 138
    IF(WORK.EQ."CHANGE") GOTO 158
    IF(WORK.EQ."NEW") GOTO 38
    IF(WORK.EQ."QUIT") GOTO 48
    TYPE"SORRY, I DON'T KNOW HOW."
25  TYPE"WHAT NEXT?"
    READ(IP,985) WORK
    GOTO 28
188  LG=.TRUE.
    CALL RAY
    GOTO 25
118  CALL LENT
    GOTO 25
128  CALL PARAX
    GOTO 25
138  CALL RED
    GOTO 25
158  CALL CHANGE
    GOTO 25
38  GOTO 18
48  CONTINUE
988  FORMAT(S1)
985  FORMAT(S7)
END
SUBROUTINE STORE
PARAMETER NRAY=96,IP=11,OF=18,NP=2
COMMON/NAME/ANAME,IREC,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,THS
COMMON/SD/SUR(18),CV(18),CC(18),TH(18),N(11,3)
COMMON/TD/DEC(18,2),TILT(18,3),RDEC(18,2),RTILT(18,3),CVY(18),CVX(18)
COMMON/TD/CVF(18)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(18)
COMMON/RAYS/R(NRAY,3)
REAL N,LNY,LNX

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Table 5. Source Code Listing of Program ICARUS (Continued).

```

TYPE"ENTER OBJECT TYPE"
READ(IF,999) OBJ
IF(OBJ.EQ."SUN") THS=1.5E+15
IF(OBJ.EQ."SUN") GOTO 15
ACCEPT"OBJECT DISTANCE IS ",THS
IF(OBJ.EQ."ANG") ACCEPT"ANGULAR FIELD(S) = ",ANY,ANX
LNY=THS*TAN(ANY/57.296)
LNK=THS*TAN(ANX/57.296)
IF(OBJ.EQ."ANG") GOTO 15
IF(OBJ.EQ."LIN") ACCEPT"LINEAR FIELD(S) = ",LNY,LNK
ANY-ATAN(LNY/THS)*57.296
ANX-ATAN(LNK/THS)*57.296
15 ACCEPT "ENTER ENTRANCE PUPIL DIAMETER ",EPD
TYPE "ENTER DIMENSIONS"
READ(IF,999) DIM
TYPE "DO YOU WISH TO SPECIFY RADII (R) OR CURVATURES (C)?"
READ(IF,998) IRQ
ACCEPT "HOW MANY LENS SURFACES ARE THERE?",LS
DO 25 I=1,LS
TYPE "ENTER SURFACE TYPE"
READ(IF,999) SUR(I)
ACCEPT "ENTER SURFACE DATA: ",CV(I),CC(I),TH(I),N(I,1),N(I,2),N(I,3)
ACCEPT"ENTER DECENTERS AND TILTS ",(DEC(I,J),J=1,2),(TILT(I,J),J=1,3)
ACCEPT"ENTER RECENTERS AND BACKTILTS ",(RDEC(I,J),J=1,2),(RTILT(I,J),
1 J=1,3)
IF(SUR(I).EQ."TOR".OR.SUR(I).EQ."TFN".OR.SUR(I).EQ."CTF") ACCEPT
1 "ENTER TORIC CURVATURES ",CVX(I),CVY(I)
IF(SUR(I).EQ."CFN".OR.SUR(I).EQ."CTF") ACCEPT"ENTER CURVATURE OF
1 FRESNEL ",CVF(I)
25 CONTINUE
IF(IRQ.EQ."C") GOTO 45
DO 35 J=1,LS
IF(CV(J).EQ.5) GOTO 22
CV(J)=1/CV(J)
22 IF(CVY(J).EQ.5) GOTO 24
CVY(J)=1/CVY(J)
24 IF(CVX(J).EQ.5) GOTO 26
CVX(J)=1/CVX(J)
26 IF(CVF(J).EQ.5) GOTO 35
CVF(J)=1/CVF(J)
35 CONTINUE
45 CALL LENW
998 FORMAT(S1)
999 FORMAT(S3)
RETURN
END
SUBROUTINE LENR
PARAMETER NRAY=96,IF=11,OF=15,NF=2
COMMON/NAME/ANAME,IREC,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNK,THS
COMMON/SD/SUR(15),CV(15),CC(15),TH(15),N(11,3)
COMMON/TD/DEC(15,2),TILT(15,3),RDEC(15,2),RTILT(15,3),CVY(15),CVX(15)
COMMON/TD/CVF(15)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(15)
COMMON/RAYS/R(NRAY,3)
REAL N,LNK,LNY
CALL FOPEN(NF,ANAME)
READ(NF,999) ANAME
READ(NF,998) OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNK,THS
DO 15 I=1,LS
READ(NF,997) SUR(I),CV(I),CC(I),TH(I),N(I,1),N(I,2),N(I,3)

```

Table 5. Source Code Listing of Program ICARUS (Continued).

```

1      READ(NF,996) (DEC(I,J),J=1,2),(TILT(I,J),J=1,3),(RDEC(I,J),J=1,2),
      (RTILT(I,J),J=1,3)
      READ(NF,995) CVY(I),CVX(I),CVF(I)
1$     CONTINUE
995    FORMAT(1X,3F1$.$)
996    FORMAT(1X,1$F1$.$)
997    FORMAT(1X,S3,6F12.$)
998    FORMAT(1X,S3,2X,S3,4F1$.$,3E1$.$)
999    FORMAT(1X,S4)
      CALL CLOSE(NF,IER)
      RETURN
      END
      SUBROUTINE LENW
      PARAMETER NRAY=96,IF=11,OF=1$,NF=2
      COMMON/NAME/ANAME,IREF,LG,IC,NCOL
      COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH$
      COMMON/SD/SUR(1$),CV(1$),CC(1$),TH(1$),N(11,3)
      COMMON/TD/DEC(1$,2),TILT(1$,3),RDEC(1$,2),RTILT(1$,3),CVY(1$),CVX(1$)
      COMMON/TD/CVF(1$)
      COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(1$)
      COMMON/RAYS/R(NRAY,3)
      REAL N,LNY,LNX
      CALL FOPEN(NF,ANAME)
      WRITE(NF,999) ANAME
      WRITE(NF,998) OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH$
      DO 1$ I=1,LS
      WRITE(NF,997) SUR(I),CV(I),CC(I),TH(I),N(I,1),N(I,2),N(I,3)
      WRITE(NF,996) (DEC(I,J),J=1,2),(TILT(I,J),J=1,3),(RDEC(I,J),J=1,2),
1      (RTILT(I,J),J=1,3)
      WRITE(NF,995) CVY(I),CVX(I),CVF(I)
1$     CONTINUE
995    FORMAT(1X,3F1$.$)
996    FORMAT(1X,1$F1$.$)
997    FORMAT(1X,S3,6F12.$)
998    FORMAT(1X,S3,2X,S3,4F1$.$,3E1$.$)
999    FORMAT(1X,S4)
      CALL CLOSE(NF,IER)
      RETURN
      END
      SUBROUTINE LENT
      PARAMETER NRAY=96,IF=11,OF=1$,NF=2
      COMMON/NAME/ANAME,IREF,LG,IC,NCOL
      COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH$
      COMMON/SD/SUR(1$),CV(1$),CC(1$),TH(1$),N(11,3)
      COMMON/TD/DEC(1$,2),TILT(1$,3),RDEC(1$,2),RTILT(1$,3),CVY(1$),CVX(1$)
      COMMON/TD/CVF(1$)
      COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(1$)
      COMMON/RAYS/R(NRAY,3)
      REAL N,LNY,LNX
      DIMENSION RD(1$)
      WRITE(OF,999) ANAME
      WRITE(OF,899)
      WRITE(OF,998) OBJ,DIM
      WRITE(OF,898)
      WRITE(OF,997) EPD,ANY,ANX,LNY,LNX,TH$
      WRITE(OF,897)
      DO 1$ I=1,LS
      IF(CV(I).EQ.$) RD(I)=1.$E+1$
      IF(CV(I).NE.$) RD(I)=1/CV(I)
1$     CONTINUE
      DO 2$ I=1,LS

```


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Table 5. Source Code Listing of Program ICARUS (Continued).

```

25 WRITE(OF,996) CV(I),RD(I),CC(I),TH(I),N(I,1),N(I,2),N(I,3)
CONTINUE
WRITE(OF,996)
K=5
DO 45 I=1,LS
SUM=DEC(I,1)**2+DEC(I,2)**2+TILT(I,1)**2+TILT(I,2)**2+TILT(I,3)**2
IF(SUM.EQ.5) GOTO 25
WRITE(OF,995) (DEC(I,J),J=1,2),(TILT(I,J),J=1,3)
25 SUM=RDEC(I,1)**2+RDEC(I,2)**2+RTILT(I,1)**2+RTILT(I,2)**2+RTILT(I,3)**2
IF(SUM.EQ.5) GOTO 35
WRITE(OF,994) (RDEC(I,J),J=1,2),(RTILT(I,J),J=1,3)
GOTO 45
35 K=K+1
45 CONTINUE
IF(K.EQ.LS) WRITE(OF,995)
K=5
WRITE(OF,994)
DO 65 I=1,LS
IF(SUR(I).NE."CFN".AND.SUR(I).NE."CTF".AND.SUR(I).NE."TOR".AND.SUR(I)
1 .NE."TFN") GOTO 55
WRITE(OF,993) CVY(I),CVX(I),CVF(I)
GOTO 65
55 K=K+1
65 CONTINUE
IF(K.EQ.LS) WRITE(OF,995)
894 FORMAT(2X,"Y CURVE",2X,"X CURVE",2X,"FRNL CURVE")
895 FORMAT(1X,"NONE")
896 FORMAT(2X,"Y DECENTER",2X,"X DECENTER",5X,"ALPHA",5X,"BETA",5X,"GAMMA")
897 FORMAT(1X,"CURVATURE",3X,"RADIUS",3X,"CONIC",2X,"THICKNESS",2X,"N1",4X,
1 "N2",4X,"N3")
898 1 FORMAT(6X,"EPD",7X,"ANGULAR FIELDS",4X,"LINEAR FIELDS",5X,"OBJ. DISTANCE
1 ")
899 FORMAT(1X,"OBJECT UNITS")
993 FORMAT(1X,3F8.6)
994 FORMAT(1X,5F11.4)
995 FORMAT(1X,5F11.4)
996 FORMAT(1X,2F15.6,F6.3,F15.4,3F7.4)
997 FORMAT(1X,5F15.4,E15.4)
998 FORMAT(3X,S3,5X,S3)
999 FORMAT(1X,S7)
RETURN
END

SUBROUTINE CHANGE
PARAMETER NRAY=96,IP=11,OP=15,NP=2
COMMON/NAME/ANAME,IREF,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,AMX,LNY,LNX,THS
COMMON/SD/SUR(15),CV(15),CC(15),TH(15),N(11,3)
COMMON/TD/DEC(15,2),TILT(15,3),RDEC(15,2),RTILT(15,3),CVY(15),CVX(15)
COMMON/TD/CVF(15)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(15)
COMMON/RAYS/R(NRAY,3)
REAL N,LNY,LNX
INTEGER RO
TYPE"WOULD YOU LIKE TO CHANGE THE OBJECT?"
READ(IF,999) ITO
IF(ITO.EQ."N") GOTO 15
TYPE"ENTER NEW OBJECT"
READ(IF,998) OBJ
15 TYPE"WOULD YOU LIKE TO CHANGE THE UNITS?"

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Table 5. Source Code Listing of Program ICARUS (Continued).

```

READ(IF,999) ITO
IF(ITO.EQ."N") GOTO 2#
TYPE"ENTER NEW UNITS"
2# READ(IF,998) DIM
TYPE"WOULD YOU LIKE TO CHANGE OBJECT DISTANCE?"
READ(IF,999) ITO
IF(ITO.EQ."N") GOTO 3#
ACCEPT"NEW OBJECT DISTANCE = ",TH#
3# TYPE"WOULD YOU LIKE TO CHANGE EPD?"
READ(IF,999) ITO
IF(ITO.EQ."N") GOTO 4#
ACCEPT"ENTER NEW EPD",EPD
4# TYPE"WOULD YOU LIKE TO CHANGE FIELD SIZE?"
READ(IF,999) ITO
IF(ITO.EQ."N") GOTO 6#
IF(OBJ.EQ."LIN") GOTO 5#
ACCEPT"ANGULAR FIELDS = ",ANY,ANX
LNY=TH#*TAN(ANY/57.296)
LNK=TH#*TAN(ANX/57.296)
GOTO 6#
5# ACCEPT"LINEAR FIELDS = ",LNY,LNX
ANY=57.296*ATAN(LNY/TH#)
ANX=57.296*ATAN(LNX/TH#)
6# TYPE"DO YOU WISH TO SPECIFY RADII (R) OR CURVATURES (C)?"
READ (IF,999) RO
TYPE"DOES THE LENS STILL HAVE",LS," SURFACES?"
READ (IF,999) ITO
IF(ITO.EQ."Y") GOTO 7#
ACCEPT"ENTER THE NUMBER OF SURFACES",LS
7# DO 9# I=1,LS
TYPE"DO YOU WISH TO CHANGE SURFACE ",I,"?"
READ(IF,999) ITO
IF (ITO.EQ."N") GOTO 9#
TYPE"ENTER SURFACE TYPE"
READ(IF,998) SUR(I)
ACCEPT"ENTER SURFACE DATA: ",CV(I),CC(I),TH(I),N(I,1),N(I,2),N(I,3)
ACCEPT"ENTER DECENTER DATA: ",(DEC(I,J),J=1,2),(TILT(I,J),J=1,3)
ACCEPT"ENTER RECENTER DATA: ",(RDEC(I,J),J=1,2),(RTILT(I,J),J=1,3)
IF(SUR(I).EQ."TOR".OR.SUR(I).EQ."TFN".OR.SUR(I).EQ."CTF")
1 ACCEPT"ENTER TORIC CURVATURES",CVY(I),CVX(I)
IF(SUR(I).EQ."CFN".OR.SUR(I).EQ."CTF") ACCEPT"ENTER PRML CURVE",CVF(I)
IF(RO.EQ."C") GOTO 9#
IF(CV(I).EQ.#) GOTO 82
CV(I)=1/CV(I)
82 IF(CVY(I).EQ.#) GOTO 84
CVY(I)=1/CVY(I)
84 IF(CVX(I).EQ.#) GOTO 86
CVX(I)= 1/CVX(I)
86 IF(CVF(I).EQ.#) GOTO 9#
CVF(I)=1/CVF(I)
9# CONTINUE
1## CALL LENW
998 FORMAT(S3)
999 FORMAT(S1)
RETURN
END
SUBROUTINE PARAX
PARAMETER NRAY=96,IF=11,OF=1#,NF=2,IM=LS+2
COMMON/NAME/ANAME,IREC,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH#
COMMON/SD/SUR(1#),CV(1#),CC(1#),TH(1#),N(11,3)

```

Table 5. Source Code Listing of Program ICARUS (Continued).

```

COMMON/TD/DEC(15,2),TILT(15,3),RDEC(15,2),RTILT(15,3),CVY(15),CVX(15)
COMMON/TD/CVP(15)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(15)
COMMON/RAYS/R(NRAY,3)
DIMENSION Y(12),CY(12),U(12),CU(12),PHI(12)
REAL N,LNY,LNX
ACCEPT "IS THIS IN COLOR 1,2,OR 3?",J
Y(5)=5
CY(5)=-LNY
U(5)=EPD/(2*TH5)
CU(5)=-LNY/TH5
PHI(5)=5
Y(1)=EPD/2
CY(1)=5
U(1)=(U(5)-Y(1)*(N(1,J)-1)*CV(1))/N(1,J)
CU(1)=CU(5)/N(1,J)
PHI(1)=(N(1,J)-1)*CV(1)
DO 15 I=2,LS+1
Y(I)=Y(I-1)+TH(I-1)*U(I-1)
CY(I)=CY(I-1)+TH(I-1)*CU(I-1)
IF(I.EQ.LS+1) GOTO 15
PHI(I)=(N(I,J)-N(I-1,J))*CV(I)
U(I)=(N(I-1,J)*U(I-1)-Y(I)*PHI(I))/N(I,J)
CU(I)=(N(I-1,J)*CU(I-1)-CY(I)*PHI(I))/N(I,J)
N(I,J)=ABS(N(I,J))
15 CONTINUE
PHI(LS+1)=5
U(LS+1)=U(LS)
CU(LS+1)=CU(LS)
WRITE(OF,999)
DO 25 I=1,LS+2
K=I-1
WRITE(OF,998) K,Y(K),CY(K),U(K),CU(K),PHI(K)
25 CONTINUE
998 FORMAT(1X,I4,5F15.6)
999 FORMAT(1X,"SURF",2X,"AXIAL Y",3X,"CHIEF Y",3X,"AXIAL U",3X,"CHIEF U",
1 5X,"POWER")
CALL LENR
RETURN
END
SUBROUTINE RAY
PARAMETER NRAY=96,IF=11,OF=15,WF=2
COMMON/NAME/ANAME,IREF,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH5
COMMON/SD/SUR(15),CV(15),CC(15),TH(15),N(11,3)
COMMON/TD/DEC(15,2),TILT(15,3),RDEC(15,2),RTILT(15,3),CVY(15),CVX(15)
COMMON/TD/CVP(15)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(15)
COMMON/RAYS/R(NRAY,3)
COMMON/TRACE/YT,XT,A,L,M,ND
COMMON/PUP/RHOY(NRAY),RHOX(NRAY)
REAL N,L,M,ND,MU,LNY,LNX
LOGICAL LG,LG2
IF(.NOT.LG) NR=NRAY
IF(.NOT.LG) GOTO 35
POBX(1)=5
POBY(1)=5
NR=1
ACCEPT "WHICH COLOR IS THE RAY, 1,2 OR 3?",JC
N,5,IC)=1
IF(OBJ.EQ."SUN") GOTO 15

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Table 5. Source Code Listing of Program ICARUS (Continued).

```

ACCEPT "ENTER FRACTIONAL OBJECT HEIGHTS",POBY(1),POBX(1)
GOTO 2$
1$ LNY=$
   LNX=$
   ANY=$
   AMX=$
2$ ACCEPT "ENTER FRACTIONAL PUPIL COORDINATES",RHOY(1),RHOX(1)
3$ DO 2$$ I=1,NR
   LG2=.FALSE.
   EX=LNX*POBX(I)
   EY=LNY*POBY(I)
   YT=RHOY(I)*EPD/2
   XT=RHOX(I)*EPD/2
   A=SQRT(THS**2+(HY-YT)**2+(EX-XT)**2)
   L=(EX-XT)/A
   M=(HY-YT)/A
   ND=THS/A
   DO 19$ J=1,LS
   IF(SUR(J).EQ."TOR".OR.SUR(J).EQ."CTF".OR.SUR(J).EQ."TFN") CALL TORT(J,LG2)
   IF(SUR(J).EQ."CON".OR.SUR(J).EQ."FNL".OR.SUR(J).EQ."CFN") CALL SYMM(J,LG2)
   IF(LG2) GOTO 2$$
19$ CONTINUE
   RXY=SQRT(XT**2+YT**2)
   IF(LG) TYPE "RAY COORDINATES AT IMAGE PLANE:  X= ",XT,"  Y= ",YT,"  R= "
1   ,RXY
   IF(LG) GOTO 2$$
   XTA(I)=XT
   YTA(I)=YT
   RA(I)=RXY
2$$ CONTINUE
   RETURN
   END

SUBROUTINE TORT(J,LG2)
PARAMETER NRAY=96,IF=11,OF=1$,NF=2
COMMON/NAME/ANAME,IREF,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,AMX,LNY,LNX,THS
COMMON/SD/SUR(1$),CV(1$),CC(1$),TH(1$),M(11,3)
COMMON/TD/DEC(1$,2),TILT(1$,3),RDEC(1$,2),RTILT(1$,3),CVY(1$),CVX(1$)
COMMON/TD/CVF(1$)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(1$)
COMMON/RAYS/R(NRAY,3)
COMMON/TRACE/YT,XT,A,L,M,ND
COMMON/PUP/ RHOY(NRAY),RHOX(NRAY)
REAL N,L,M,ND,MU,LNY,LNX
LOGICAL LG,LG2
Y=Y+DEC(J,1)-RDEC(J,1)
X=X+DEC(J,2)-RDEC(J,2)
N= SIN(ASIN(N)+TILT(J,1)/59.29578)
M= SIN(ASIN(M)+TILT(J,2)/57.29578)
L= SIN(ASIN(L)+TILT(J,3)/57.29578-RTILT(J,3)/57.29578)
M= SIN(ASIN(M)-RTILT(J,2)/57.29578)
N= SIN(ASIN(N)-RTILT(J,1)/57.29578)
IF (SUR(J).EQ."CTF") GOTO 1$
BX=CVX(J)*XT**2
BY=CVY(J)*YT**2
CX=ND-CVX(J)*L*XT
CY=ND-CVY(J)*M*YT
DSX=CX**2-(CVX(J)*XT)**2
DSY=CY**2-(CVY(J)*YT)**2
GOTO 2$

```

Table 5. Source Code Listing of Program ICARUS (Continued).

```

1#    BX=CVF(J)*(XT**2+YT**2)
      BY=BX
      CX=ND-CVF(J)*(L*XT+M*YT)
      CY=CX
      DSX=CX**2-CVF(J)*BX
      DSY=DSX
2#    IF(ABS(DSX).LE.1E-1#) DSX=#
      IF(ABS(DSY).LE.1E-1#) DSY=#
      DX=SQRT(DSX)
      DY=SQRT(DSY)
      A=(BX/(CX+DX)+BY/(CY+DY))/2
      IF(SUR(J).EQ."TFN") A=#
      XS=XT+A*L
      YS=YT+A*M
      ZS=A*ND
      CSIX=DX
      CSIY=DY
      MU=N(J-1,IC)/ABS(N(J,IC))
      DEXS=1-MU**2*(1-CSIX**2)
      DEYS=1-MU**2*(1-CSIY**2)
      IF(DEXS.LE.#.OR.DEYS.LE.#) GOTO 7#
      DEX=SQRT(DEXS)-MU*CSIX
      DEY=SQRT(DEYS)-MU*CSIY
      ALPHA=-CVX(J)*XS
      BETA=-CVY(J)*YS
      L=MU*L+DEX*ALPHA
      M=MU*M+DEY*BETA
      ND=SQRT(1-L**2-M**2)
      XT=XS+L*(TH(J)-ZS)/ND
      YT=YS+M*(TH(J)-ZS)/ND
      A=SQRT((TH(J)-ZS)**2+(YT-YS)**2+(XT-XS)**2)
      GOTO 95
7#    IF(LG) TYPE"TOTAL INTERNAL REFLECTION AT SURFACE",J
      GOTO 9#
8#    IF(LG) TYPE"RAY MISSED SURFACE",J
9#    LG2=.TRUE.
95    RETURN
      END

SUBROUTINE SYMM(J,LG2)
PARAMETER NRAY=96,IF=11,OF=1#,NF=2
COMMON/NAME/ANAME,IREF,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH#
COMMON/SD/SUR(1#),CV(1#),CC(1#),TH(1#),N(11,3)
COMMON/TD/DEC(1#,2),TILT(1#,3),RDEC(1#,2),RTILT(1#,3),CVY(1#),CVX(1#)
COMMON/TD/CVF(1#)
COMMON/RAYS/POBY(NRAY),POBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(1#)
COMMON/RAYS/R(NRAY,3)
COMMON/TRACE/YT,XT,A,L,M,ND
COMMON/PUP/ RHOY(NRAY),RHOX(NRAY)
REAL N,L,M,ND,MU,LNY,LNX
LOGICAL LG,LG2
Y=Y+DEC(J,1)-RDEC(J,1)
X=X+DEC(J,2)-RDEC(J,2)
N=SIN(ASIN(N)+TILT(J,1)/57.29578)
M=SIN(ASIN(M)+TILT(J,2)/57.29578)
L=SIN(ASIN(L)+TILT(J,3)/57.29578-RTILT(J,3)/57.29578)
M=SIN(ASIN(M)-RTILT(J,2)/57.29578)
N=SIN(ASIN(N)-RTILT(J,1)/57.29578)
IF(SUR(J).EQ."CFN") GOTO 1#
B=CV(J)*(XT**2+YT**2)

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Table 5. Source Code Listing of Program ICARUS (Continued).

```

C=ND-CV(J)*(L*XT+M*YT)
DS=C*C-CV(J)*B*(1+CC(J)*ND*ND)
GOTO 28
18 B=CVF(J)*(XT**2+YT**2)
C=ND-CVF(J)*(L*XT+M*YT)
DS=C*C-CVF(J)*B
28 IF(ABS(DS).LE.1E-18) DS=8
D=SQRT(DS)
A=B/(C+D)
IF(OBJ.EQ."FNL") A=8
XS=XT+A*L
YS=YT+A*M
ZS=A*ND
E2=1/(1-2*CV(J)*CC(J)*ZS)
E=SQRT(E2)
CSI=D*E
MU=N(J-1,IC)/ABS(N(J,IC))
DELS=1-MU**2*(1-CSI**2)
IF(DELS.LT.8) GOTO 78
DEL=SQRT(DELS)-MU*CSI
ALPHA=-CV(J)*E*XS
BETA=-CV(J)*E*YS
GAMMA=(1-CV(J)*(CC(J)+1)*ZS)*E
L=MU*L+DEL*ALPHA
M=MU*M+DEL*BETA
ND=MU*ND+DEL*GAMMA
XT=XS+L*(TH(J)-ZS)/ND
YT=YS+M*(TH(J)-ZS)/ND
A=SQRT((TH(J)-ZS)**2+(YT-YS)**2+(XT-XS)**2)
GOTO 95
78 IF(LG) TYPE"TOTAL INTERNAL REFLECTION AT SURFACE ",J
GOTO 98
88 IF(LG) TYPE "RAY MISSED SURFACE ",J
98 LG2=.TRUE.
95 RETURN
END

SUBROUTINE RED
PARAMETER NRAY=96,IF=11,OF=18,JP=2
COMMON/NAME/ANAME,IREC,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH8
COMMON/SD/SUR(18),CV(18),CC(18),TH(18),N(11,3)
COMMON/TD/DEC(18,2),TILT(18,3),RDEC(18,2),RTILT(18,3),CVY(18),CVX(18)
COMMON/TD/CVF(18)
COMMON/RAYS/FOBY(NRAY),FOBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(18)
COMMON/RAYS/R(NRAY,3)
COMMON/PUP/RHOY(NRAY),RHOX(NRAY)
REAL N,LNY,LNX
LOGICAL LG
DIMENSION FY(12),FX(12),RY(8),RX(8)
DATA FY/.31,8,-.31,8,.57,8,-.57,8,.89,8,-.89,8/
DATA FX/8,.31,8,-.31,8,.57,8,-.57,8,.89,8,-.89/
DATA RY/.7,8,-.7,8,1,8,-1,8/
DATA RX/8,.7,8,-.7,8,1,8,-1/
LG=.FALSE.
LNX=4.36E+7
LNY=4.36E+7
DO 28 I=1,12

```

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Table 5. Source Code Listing of Program ICARUS (Continued).

```

DO 18 J=1,8
K=8*(I-1)+J
FOBY(K)=FY(I)
FOBX(K)=FX(I)
RHOY(K)=RY(J)
RHOX(K)=RX(J)
18 CONTINUE
28 CONTINUE
ACCEPT"HOW MANY COLORS WOULD YOU LIKE? ",NCOL
DO 48 J=1,NCOL
CALL RAY
DO 38 I=1,NRAY
R(I,J)=RA(I)
38 CONTINUE
48 CONTINUE
CALL SORT
WRITE(OF,999)
DO 58 I=1,18
J=18*I
WRITE(OF,998) J,RAD(I)
58 CONTINUE
998 FORMAT(7X,I3,7X,F18.4)
999 FORMAT(1X,"PERCENT ENERGY",5X,"RADIUS")
RETURN
END
SUBROUTINE SORT
PARAMETER NRA=96,IF=11,OF=18,NF=2
COMMON/NAME/ANAME,IREF,LG,IC,NCOL
COMMON/OD/OBJ,DIM,EPD,LS,ANY,ANX,LNY,LNX,TH8
COMMON/SD/SUR(18),CV(18),CC(18),TH(18),N(11,3)
COMMON/TD/DEC(18,2),TILT(18,3),RDEC(18,2),RTILT(18,3),CVY(18),CVX(18)
COMMON/TD/CVF(18)
COMMON/RAYS/FOBY(NRAY),FOBX(NRAY),XTA(NRAY),YTA(NRAY),RA(NRAY),RAD(18)
COMMON/RAYS/R(NRAY,3)
NRA=NRAY*NCOL
DIMENSION A(288)
REAL N,LNY,LNX
DO 68 I=1,NRA
A(I)=0
DO 28 K=1,NCOL
DO 18 J=1,NRAY
A(I)=AMAX1(A(I),R(J,K))
18 CONTINUE
28 CONTINUE
DO 48 K=1,NCOL
DO 38 J=1,NRAY
IF(A(I).NE.R(J,K)) GOTO 38
R(J,K)=0
GOTO 68
38 CONTINUE
48 CONTINUE
68 CONTINUE
M=IFIX(NRA/18+.5)
DO 78 I=1,9
RAD(I)=A(NRA+1-M*I)
78 CONTINUE
RAD(18)=A(1)
RETURN
END

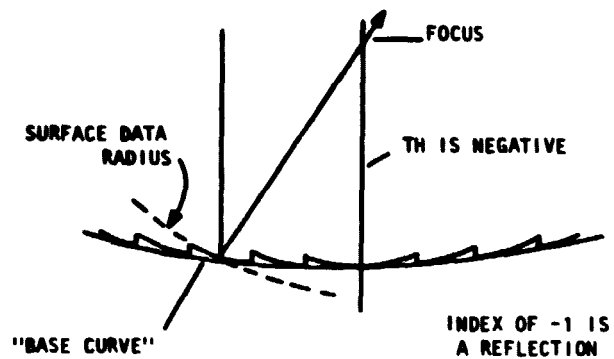
```

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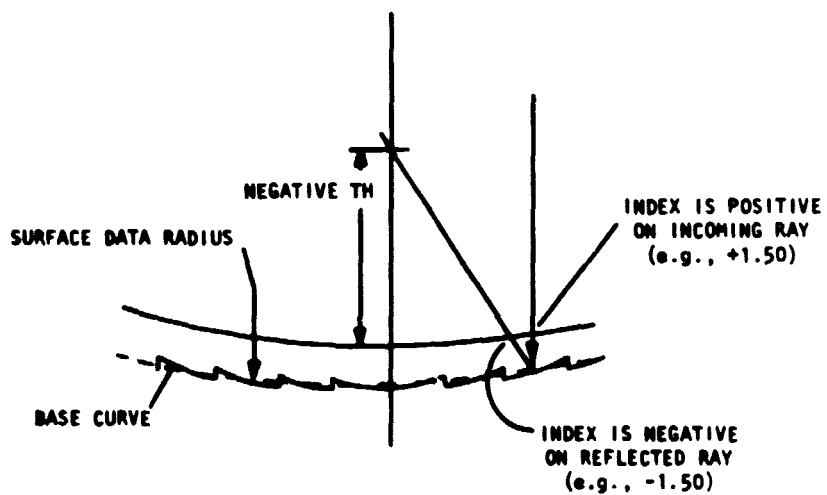
APPENDIX B

EXAMPLES OF LENSES THROUGH WHICH RAYS CAN BE TRACED

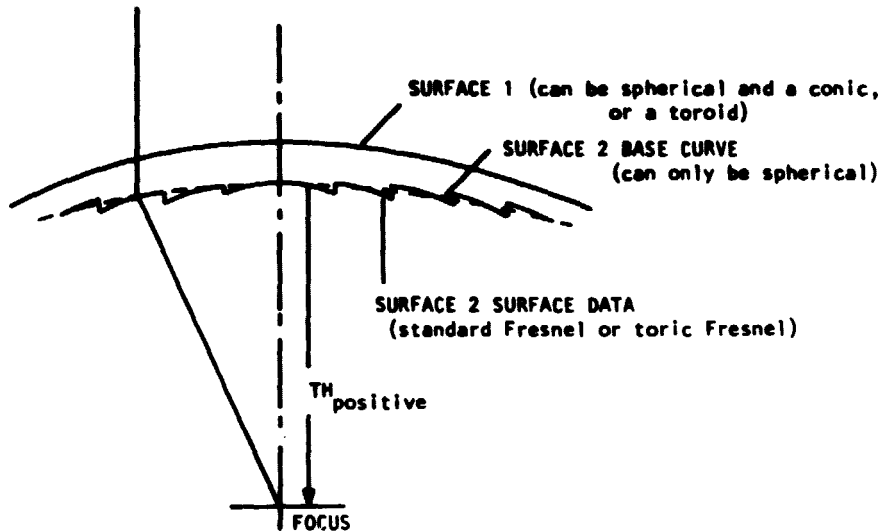
1. Front Surface Reflective Fresnel



2. Rear Surface Reflective Fresnel

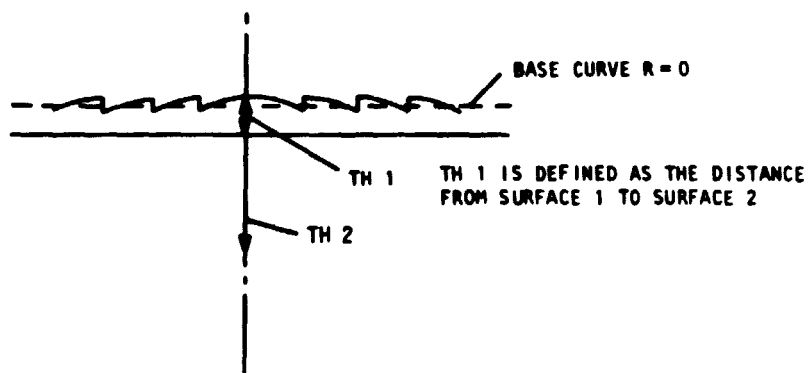


3. Rear Surface Transmissive Fresnel



Note that, when "Fresnel" is specified, the limitation of only a spherical base curve enters. This limitation can be removed, but isn't in this edition. The Fresnel elements, as specified by the "surface data," can be conic, toric, etc.

4. Flat Transmissive Fresnel



Note that a flat surface can be designated as a conic even though it is flat, and it will be treated as an asphere with the departure from the plane being the same as the departure of the corresponding conic from the sphere whose curvature it approximates at its vertex.